

**Report No.:** GM/23/279G **Date:** 07/12/2023 To Kalgidhar Trust, Baru Sahib. Subject: Geotechnical investigation report for proposed Akal nursing college Building at Baru Sahib. Please find enclosed herewith the bearing capacity report of soil for the above said project. Rev. & App. by



**Authorized Signatory** 



CIN: U74999PB2018PTCO47685



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Project: Geotechnical investigation report for proposed Akal nursing college Building at Baru Sahib.

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GSTIN: 03AAHCG2565L1ZI



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**I.Discipline:** Mechanical Testing **Group:** Soil & Rock (Field Testing)

#### 1.0 INTRODUCTION

Geo-Media Engineering and Consultancy Services (Geo-Media) Pvt. Ltd. presents herein our Geotechnical investigation report for proposed Akal nursing college Building at Baru Sahib. The purpose of this report is to assess subsurface conditions in order to provide geotechnical comments and recommendations for soil characteristics, bearing capacity and earth pressure. Attachments to this report include soil bore-logs.

# 2.0 FIELD INVESTIGATIONS 2.1 BORE HOLE LOCATION:

The locations of bore holes were given by Mr. Vikramjeet Singh. Three bore hole designated as BH-1 to BH-03 were done to carry out the desired investigations

#### 2.2 STANDARD PENETRATION TEST

According to IS code 2131-1981 Standard penetration test was conducted at each bore hole and samples were collected at an interval of 1.5m or at a depth where there is change in strata. N values were recorded at required depths as per the code up to significant depth. N values observed in the field are corrected for both the corrections

• Overburden Pressure Correction  $N_n = C_n \times N$ 

Where  $C_n$  is correction for overburden pressure, N = Observed no of blows.

• Dilatancy Correction: This correction is required for fine sands below water table

 $N_C = 15 + (N_n - 15) / 2$  When  $N_n > 15$   $N_C = corrected value$ .

## 3.0 LABORATORY INVESTIGATIONS

#### 3.1 INDEX PROPERTIES

Following Index Properties of the soil samples collected from various depths are determined for the classification of soil.

- Particle size distribution
- Relative density
- Atterbergs limits

#### 3.2 ENGINEERING PROPERTIES

Following Engineering Properties are determined in the laboratory from the tests mentioned against them.

- Shear Strength (c' and  $\Phi'$  from direct shear test and triaxial shear test)
- Permeability (k from constant and variable head permeability test)
- Compressibility (Compaction and Consolidation test)



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#### 4.0 CALCULATION OF BEARING CAPACITY

The soil can fail either in shear or settlement. Net allowable bearing capacity will be determined with both the cases. The criteria, with minimum value will govern the bearing capacity of soil.

#### 4.1 BEARING CAPACITY BASED ON SHEAR

Net ultimate bearing capacity  $q_{nu}$  as per IS code 6403--1981.

 $q_{nu} = 2/3 \text{ c'N'}_c \text{ S}_c d_c i_c \text{ i} + \Upsilon D_f (N_q'-1) \text{ S}_q d_q i_q + 0.5 \Upsilon BN'_{\gamma} S_{\gamma} d_{\gamma} i_{\gamma} W' \text{ (local shear failure)}$ 

 $q_{nu} = cN_C \ S_c \ d_c \ i_c + \Upsilon \ D_f \ (N_q - 1) \ S_q \ d_q \ i_q + \ 0.5 \ \Upsilon \ B \ N_\gamma \ S_\gamma \ d_\gamma \ i_\gamma \ W' \quad (General \ shear \ failure)$ 

Net safe bearing capacity  $q_{ns} = q_{nu} / 2.5$   $\Phi' = tan^{-1} (2/3tan\Phi)$ 

 $N'_c$ , N'q,  $N'\gamma$  are bearing capacity factors for local shear failure.

N<sub>c</sub>, Nq, Ny are bearing capacity factors for general shear failure

 $d_c$ ,  $d_q$ ,  $d_\gamma$  are the depth factors

ic, iq, iγ are the Inclination factors

 $S_c$ ,  $S_q$ ,  $S_\gamma$  are the Shape factors

	Size (m)		1.50 x 1.50						
Assumed data of Foundation	Туре		Square						
1 oundation	Depth (m) w.r.t. Top of Bore Hole	1.00							
Pro	operties \	BH-1	BH-2	ВН-3					
	w'	0.50	0.50	0.50					
С	' (t/m²)	0.00	0.00	0.00					
γ	(g/cc)	1.62	1.70	1.70					
	Ф°	26.50	29.00	29.00					
	Φ'°	18.38	18.38 20.28						
	Nc	13.59	15.20	15.20					
	Nq	5.61	6.64	6.64					
	Νγ	4.51	5.70	5.70					
	Sc	1.30	1.30	1.30					
	Sq	1.20	1.20	1.20					
	Sr	0.80	0.80	0.80					
	dc	1.184	1.192	1.1835					
	dq=dγ	1.092	1.096	1.092					
qı	u (t/m²)	12.18	12.18 15.80						
qr	as (t/m²)	4.87	6.32	6.29					

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#### 4.2 BEARING CAPACITY BASED ON SETTLEMENT CRITERIA

Both overburden and dilatancy corrections are required to be applied to the observed as per IS2131-1981. Net allowable safe bearing pressure is calculated as the allowable limits given in IS code 8009 part 1 and water table correction factor is taken into consideration.

#### **BH-1**

Depth from		Over Burden	_		
Top of Bore	N	Pressure	$C_n$	$N_n$	$N_c$
Hole (m)		Kg /cm <sup>2</sup>			
1.00	3	0.162	1.610	4.83	4.83
1.50	4	0.244	1.474	5.90	5.90
2.00	6	0.327	1.376	8.26	8.26
3.00	9	0.499	1.235	11.11	11.11
4.50	10	0.761	1.093	10.93	10.93
6.00	89	1.073	0.978	87.06	87.06
7.50	113	1.388	0.892	100.81	100.81
9.00	Refusal	1.706	0.823		
10.00	Refusal	1.918	0.784		

#### **BH-2**

D11-2												
Depth from		Over Burden										
Top of Bore	N	Pressure	$C_n$	$N_n$	$N_c$							
Hole (m)		Kg /cm <sup>2</sup>										
1.00	8	0.170	1.594	12.75	12.75							
1.50	75	0.274	1.435	107.65	107.65							
2.00	6	0.357	1.347	8.08	8.08							
3.00	8	0.527	1.216	9.73	9.73							
4.50	25	0.819	1.069	26.71	26.71							
6.00	86	1.131	0.961	82.61	82.61							
7.50	121	1.448	0.878	106.25	106.25							
9.00	Refusal	1.766	0.812	_	_							
10.00	Refusal	1.978	0.774	<del></del>	_							

#### **BH-3**

Depth from Top of Bore Hole (m)	N	Over Burden Pressure Kg /cm <sup>2</sup>	Cn	$N_n$	N <sub>c</sub>						
1.00	8	0.170	1.594	12.75	12.75						
1.50	15	0.263	1.449	21.74	21.74						
2.00	15	0.355	1.348	20.22	20.22						

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Depth from Top of Bore Hole (m)	N	Over Burden Pressure Kg /cm <sup>2</sup>	C <sub>n</sub>	N <sub>n</sub>	$N_{c}$
3.00	20	0.545	1.205	24.10	24.10
4.50	85	0.823	1.067	90.71	90.71
6.00	95	1.115	0.965	91.71	91.71
7.50	116	1.430	0.882	102.33	102.33
9.00	Refusal	1.748	0.815		_
10.00	Refusal	1.960	0.777		

Bore Holes	Nc (Avg)	Net allowable pressure qnp (t/m²)
BH-1	8.21	12.98
BH-2	32.99	74.76
BH-3	33.90	77.04

#### 5.0 NET ALLOWABLE BEARING CAPACITY

The net safe bearing capacity is the least of the bearing capacity based on above two criteria and its value is given in the following table.

Bore Hole	Depth of Foundation w.r.t top of Bore Hole (m)	Size of foundation (m)	Type of Foundation	Net safe bearing capacity q <sub>ns</sub> (t/m²) From shear criteria	Net safe pressure  q <sub>np</sub> (t/m²)  From Settlement  criteria	Net Allowable Bearing Capacity (t/m²)	
BH-1	1.00	1.50 x 1.50	Square	4.87	12.98	4.87	
BH-2	1.00	1.50 x 1.50	Square	6.32	74.76	6.32	
ВН-3	1.00	1.50 x 1.50	Square	6.29	77.04	6.29	

## **6.0 RECOMMENDATIONS**

i) Net allowable bearing capacity is given in following table.

Sr. No.	Depth of Foundation w.r.t Top of Bore Hole (m)	Size of foundation (m)	Type of Foundation	Net Allowable Bearing Capacity (t/m²)	Gross Safe Bearing Capacity (t/m²)
1	1.00	1.50	Strip	4.46	6.08
2	1.00	2.00	Strip	4.75	6.37
3	1.00	1.50 x 1.50	Square	4.87	6.49
4	1.00	2.00 x 2.00	Square	5.08	6.70

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Sr. No.	Depth of Foundation w.r.t Top of Bore Hole (m)	Size of foundation (m)	Type of Foundation	Net Allowable Bearing Capacity (t/m²)	Gross Safe Bearing Capacity (t/m²)
5	1.00	3.00 x 3.00	Square	5.58	7.20
6	1.50	1.50	Strip	6.77	9.21
7	1.50	2.00	Strip	7.00	9.44
8	1.50	1.50 x 1.50	Square	7.59	10.03
9	1.50	2.00 x 2.00	Square	7.70	10.14
10	1.50	3.00 x 3.00	Square	8.13	10.57
11	2.00	1.50	Strip	9.91	13.18
12	2.00	2.00	Strip	10.02	13.29
13	2.00	1.50 x 1.50	Square	11.26	14.53
14	2.00	2.00 x 2.00	Square	11.21	14.48
15	2.00	3.00 x 3.00	Square	11.53	14.80
16	2.70	3.00	Strip	14.67	19.14
17	3.00	1.50	Strip	17.17	22.44
18	3.00	2.00	Strip	16.81	22.08
19	3.00	1.50 x 1.50	Square	19.86	25.13
20	3.00	2.00 x 2.00	Square	19.22	24.49
21	3.00	3.00 x 3.00	Square	18.97	24.24

- ii) Top of bore hole is equal to NSL.
- iii) The Ground Water table has not been encountered upto the depth of soil exploration.
- iv) Allowable settlement is taken as 50mm for isolated foundation.

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- 1. This certificate refers only to the particular site location of testing.
- 2. This certificate shall not be reproduced, except in full, unless written permission is obtained.
- 3. The test results reported in this certificate are valid for the stated conditions of measurements.
- 4. Sample will be destroyed after three months from the date of the issue of the test report unless otherwise specified.
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## 7.0 Bore Log Chart

Ref No SI	<b>Ref. No.</b> SRF/23/1122C					<b>Ref. Dated:</b> 29.11.23			Date of Field Testing: 26.11.2023					No. TC11794	AS THE THE PART OF		
ici. No. Si				IXCI.	233. 233. 27.11.20				Ground water table: - not encountered					<b>Bore Hole No.:-</b> 01 of 03			
Depth from Top	Nature of	f	Syr	mbolic	Grai	n Size Aı	nalysis	· ·		Bulk unit weight	Тє		S.P.T Value (Observed)	IS: Classification			
of Bore Hole(m)	Sample	R	Repre	sentation	Gravel (%)	Sand (%)	Silt & Clay (%)	L.L	P.L	P.I	$\Upsilon$ (t/m <sup>3</sup> )	C' (t/m <sup>2</sup> )	φ <b>′</b> °	` '	15.	. Clas	sification
1.00	SPT/DS				0.00	63.21	36.79	NP	NP	NP	1.62	0.00	26.50	3	SM		
1.50	SPT/DS				0.00	52.76	47.24	NP	NP	NP	1.63	0.00	27.00	4	SM		
2.00	SPT/DS				0.00	51.28	48.72	NP	NP	NP	1.66	0.00	28.50	6	SM		
3.00	SPT/DS				0.00	56.75	43.25	NP	NP	NP	1.72	0.00	29.25	9	SM	S	ILTY SAND
4.50	SPT				0.00	55.94	44.06	NP	NP	NP	1.75			10	SM		
6.00	SPT				15.43	62.75	21.82	NP	NP	NP	2.08			89	SM		
7.50	SPT				33.65	50.27	16.08	NP	NP	NP	2.10			113	SM		
9.00							Weathered R	Rock			2.12			Refusal	13.7	ontho	red Rock
10.00						_	Weathered R	Rock			2.12			Refusal	weathe		TOU NOOK



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Ref. No. SI	RF/23/112	22C	Ref. 1	Date of Field Testing: 27.11.2023						No. TC11794	The Control of the Co				
				Grou	Ground water table: - not encountered					ore Hole No.	:- 02 of 0	)3	γ-11794		
Depth from Top	Nature of	Grain Size Analysis  Consistency Characteristics (%)  Bulk unit Direct Shear Characteristics (%)  Test			S.P.T Value (Observed)	IS	IS: Classification								
of Bore Hole(m)	Sample	Representation	Gravel (%)	Sand (%)	Silt & Clay (%)	L.L	P.L	P.I	$\Upsilon$ (t/m <sup>3</sup> )	C' (t/m <sup>2</sup> )	φ <b>′</b> °	(N Value)	is: Cias		ssincation
1.00	SPT/DS		0.00	72.10	27.90	NP	NP	NP	1.70	0.00	29.00	8	SM	S	ILTY SAND
1.50	SPT/DS		55.12	41.02	3.86	NP	NP	NP	2.07	0.00	29.00	75	GP	GP POORLY GR GRAVE	
2.00	SPT/DS		0.00	79.98	20.02	NP	NP	NP	1.66	0.00	28.50	6	SM	<b>C</b> T	ILTY SAND
3.00	SPT/DS		0.00	53.14	46.86	NP	NP	NP	1.70	0.00	29.00	8	SM	۵.	ILI I SAND
4.50	SPT		32.61	65.19	2.20	NP	NP	NP	1.95			25	SP	POO	RLY GRADED
6.00	SPT		0.00	98.07	1.93	NP	NP	NP	2.08			86			SAND
7.50	SPT		56.12	40.15	3.73	NP	NP	NP	2.11			121	GP	POO	RLY GRADED GRAVEL
9.00					Weathered R	lock			2.12			Refusal	V	/eathe	red Rock
10.00					Weathered R	lock			2.12			Refusal		cathe	ICU KOCK



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<b>Ref. No.</b> SRF/23/1122C			<b>Ref. Dated:</b> 29.11.23		Date of Field Testing: 29.11.2023				ULR	ULR No. TC1179423000000604F			A STATE OF THE STA		
					Ground water table: - not e			- not encou	encountered I		<b>Bore Hole No.:-</b> 03 of 03		)3	पारत । पारत । TC-11794	
Depth from Top			Grain Size Analysis		Characteristics (%)		Bulk unit weight	Те		S.P.T Value (Observed)	IS: Classification				
of Bore Hole(m)	Sample	Representation	Gravel (%)	Sand (%)	Silt & Clay (%)	L.L	P.L	P.I	$\Upsilon$ (t/m <sup>3</sup> )	$C'$ $(t/m^2)$	φ <b>′</b> °	(N Value)		is. Classification	
1.00	SPT/DS		5.12	77.15	17.73	NP	NP	NP	1.70	0.00	29.00	8	SM	Sl	LTY SAND
1.50	SPT/DS		70.19	25.21	4.60	NP	NP	NP	1.85	0.00	29.75	15	GP	POORLY GRADED GRAVEL	
2.00	SPT/DS		0.00	98.78	1.22	NP	NP	NP	1.85	0.00	29.75	15	SP		
3.00	SPT/DS		12.15	86.51	1.34	NP	NP	NP	1.90	0.00	30.50	20	SP	POORLY GRADED SAND	
4.50	SPT		31.54	64.44	4.02	NP	NP	NP	1.85			85	SP		
6.00	SPT		62.57	35.48	1.95	NP	NP	NP	1.95			95	GP	POORLY GRADED GRAVEL	
7.50	SPT		51.21	45.75	3.04	NP	NP	NP	2.10			116	GP		
9.00	_		Weathered Rock				2.12			Refusal	Weathered Rock				
10.00			Weathered Rock				2.12			Refusal	weamered Rock				

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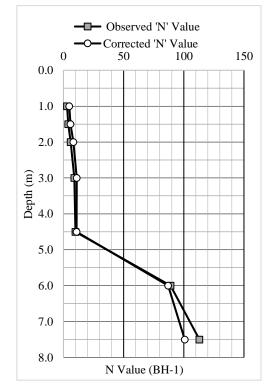


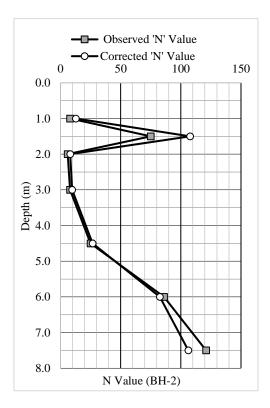
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## 8.0 Observed SPT 'N'-Value and Corrected 'N'-value Graph

Depth from Top of Bore	Observed	'N' Value	Corrected 'N' Value			
Hole (m)	BH-1	BH-2	BH-1	ВН-2		
1.00	3	8	4.83	12.75		
1.50	4	75	5.90	107.65		
2.00	6	6	8.26	8.08		
3.00	9	8	11.11	9.73		
4.50	10	25	10.93	26.71		
6.00	89	86	87.06	82.61		
7.50	113	121	100.81	106.25		
9.00	Refusal	Refusal	_			
10.00	Refusal	Refusal				



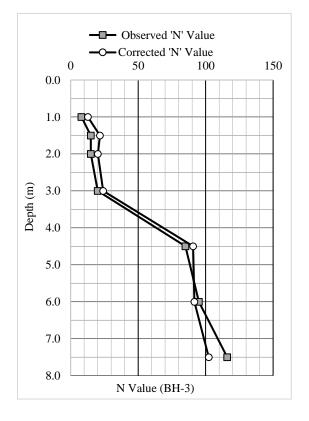




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Depth from Top of	Observed 'N' Value	Corrected 'N' Value		
Bore Hole (m)	ВН-3	ВН-3		
1.00	8	12.75		
1.50	15	21.74		
2.00	15	20.22		
3.00	20	24.10		
4.50	85	90.71		
6.00	95	91.71		
7.50	116	102.33		
9.00	Refusal	_		
10.00	Refusal	_		





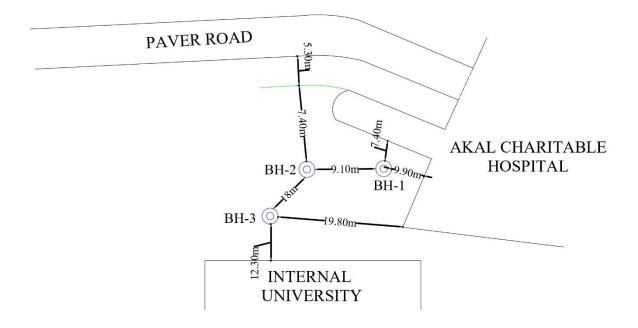


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#### 9.0 Site Plan

AKAL NURSING COLLEGE





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## Appendix I

 $N'_{C}$ ,  $N_{q}'$ ,  $N'_{\gamma}$  = Bearing capacity factors for local shear failure.  $N_{C}$ ,  $N_{q}$ ,  $N_{\gamma}$ , = Bearing capacity factors for general shear failure.

 $S_{C, S_q, S_{\gamma}} =$  Shape factors.  $d_{C, d_q, d_{\gamma}} =$  Depth factors.

W' = Water table correction factor.

 $egin{array}{lll} N & = & Observed SPT \ value. \\ N_N & = & Normalised SPT \ value. \\ C_N & = & Correction \ factor. \\ N_c & = & Corrected \ N \ value \\ \Upsilon & = & Bulk \ unit \ weight. \\ \end{array}$ 

Υ' = Submerged unit weight

 $\Upsilon_d$  = Dry unit weight.

 $\Upsilon_{sat}$  = Saturated unit weight. G = Specific gravity of soil.

LL = Liquid Limit.

PL = Plastic Limit.

PI = Plasticity Index.

GSF = General shear failure.

LSF = Local shear failure.

 $q_u$  = Unconfined compressive strength.

c<sub>u</sub> = Un-drained shear strength

Compression index  $c_{c}$ = В Width of foundation = Length of foundation L Depth of foundation  $D_{\rm f}$ =Thickness of clayey layer Η = Top width of sandy layer  $B_t$ Thickness of sandy layer Η =Effective surcharge = q

 $\Phi'$  = Angle of shearing resistance

 $\Phi'_{\rm m}$  = Mobilised angle of shearing resistance

 $\begin{array}{lll} c' & = & Cohesion\ intercept \\ SSWL & = & Sub\ soil\ water\ level \\ q_u & = & Ultimate\ bearing\ capacity \\ q_{nu} & = & Net\ ultimate\ bearing\ capacity \end{array}$ 

 $q_{ns}$  = Net safe bearing capacity against shear failure  $q_{np}$  = Net safe bearing pressure against settlement failure

q<sub>a</sub> = Allowable bearing capacity

WT = Water Table

GW = Well graded gravels
GP = poorly graded gravels

GM = Silty gravels

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GC Clayey gravels = SW Well graded Sand = SP poorly graded Sand =Silty Sand SM = SC Clayey Sand =Clay of low compressibility CL Silt of low compressibility ML =Clay of medium compressibility CI = Silt of medium compressibility MI = Clay of high compressibility CH = Silt of high compressibility MH Total settlement  $S_{t}$ Allowable settlement  $\mathbf{S}_{\mathbf{a}}$ 

s<sub>o</sub> = Settlement due to net unit foundation loading intensity

BH = Bore hole

OBP = overburden pressure NSL = Natural surface level

 $C_1$  = Correction factor for depth of foundation embedment

 $C_2$  = Correction factor for creep in soils

 $\begin{array}{lll} I_z & = & Influence \ factor \\ E_s & = & Modulus \ of \ elasticity \\ ESL & = & Existing \ Surface \ Level \end{array}$ 



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## Appendix-II

I. S. Codes

Following IS Codes are used for the testing and calculations in this report.

1.	IS:1904-1986,	"Design & Construction of Foundation in Soils, General				
	Requirements."					
2.	IS:2131-1981,	"Method for Standard Penetration Test for Soil."				
3.	IS:2720-Part-2 1973,	"Determination of Water Content."				
4.	IS:2720-Part-3 1980,	"Determination of Specific gravity-Fine-grained soils."				
5.	IS:2720-Part-4 1975,	"Grain size analysis."				
6.	IS:2720-Part-5 1970,	"Determination of Liquid and Plastic Limits."				
7.	IS:2720-Part-13 1982,	"Direct Shear Test"				
8.	IS:2720-Part-15 1986,	"Determination of Consolidation Properties."				
9.	IS:6403-1981,	"Code of Practice for Determination of Bearing Capacity of Shallow				
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10.	IS:8009-Part 2-1980,	"Code of Practice for calculations of settlement of Foundation-Deep				
		Foundation subjected To Symmetrical Static Vertical Loading."				
11.	IS:8763-1978,	"Guide for Undisturbed Sampling of Sand."				
12.	IS:9259-1979,	"Specifications for Liquid Limit Apparatus for Soils."				
13.	3. IS:9640-1981, "Specifications for Split-spoon Sampler."					

\*\*\*END OF REPORT\*\*\*

